

Digital Signal Processing

Chap 7. Filter Design Techniques

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Filters



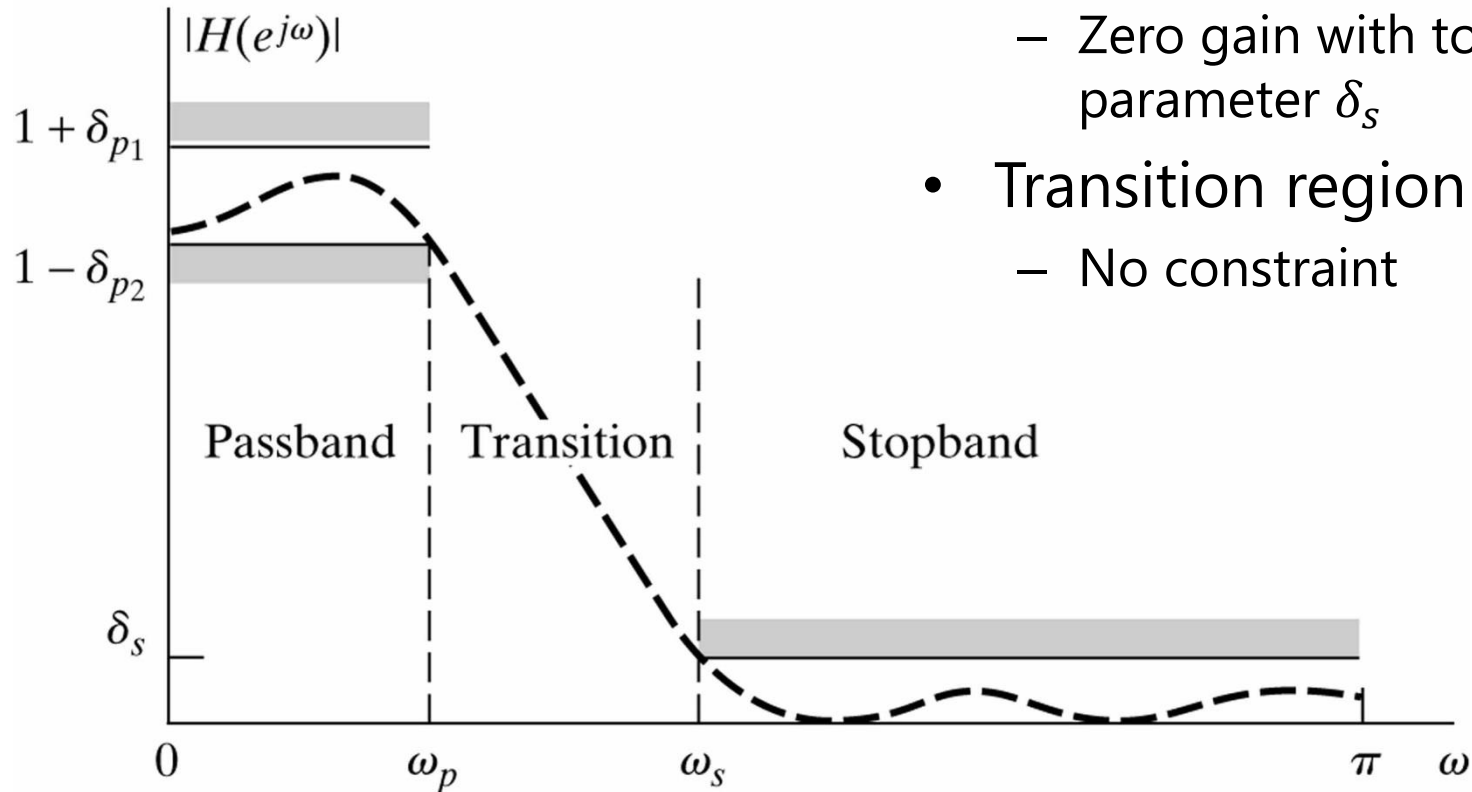
- **Allow some parts** of input materials to pass through it
- but **block the other parts**

Summary

- Filter specifications
- Design of DT IIR filters from CT filters
 - Impulse invariance
 - Bilinear transformation
 - Ex) Butterworth, Chebyshev, Elliptic filters
- There are many more filters and their design techniques, which are beyond the scope of this course.

Filter Specifications

Tolerance Scheme

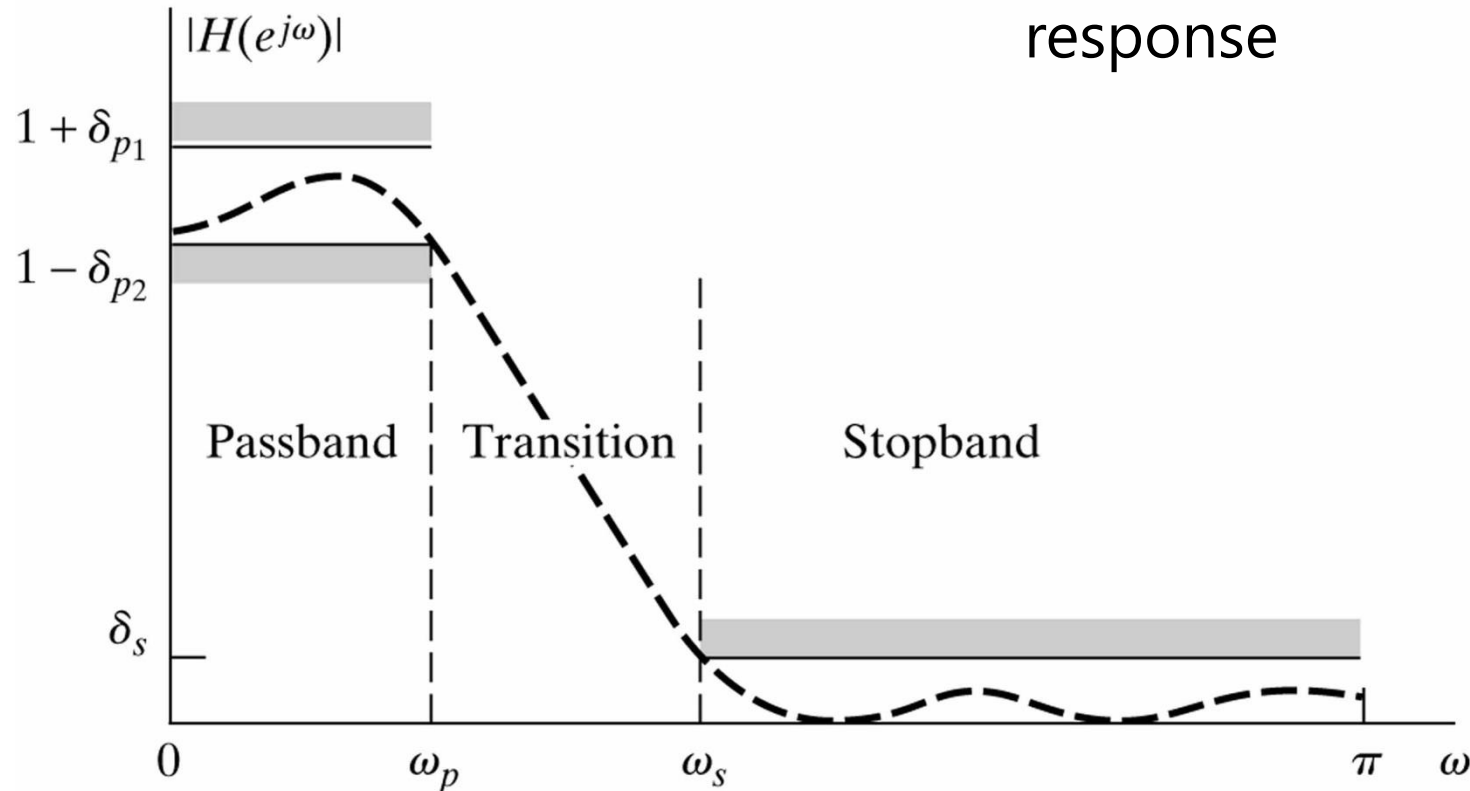


- Passband
 - Unity gain with tolerance parameters δ_{p_1} and δ_{p_2}
- Stopband
 - Zero gain with tolerance parameter δ_s
- Transition region
 - No constraint

Filter Specifications

Tolerance Scheme

- We focus on the case of lowpass filter with no constraint on the phase response



Design of DT filters from CT filters

- Historically, CT filters had been more intensively researched than DT filters
- It was natural to consider converting CT filters into DT filters
- Two such methods are
 - Impulse invariance
 - Bilinear transformation

Impulse Invariance

- Recall the C/D conversion
 - $x[n] = x_c(nT)$
 - $X(e^{j\omega}) = \frac{1}{T} \sum_{k=-\infty}^{\infty} X_c \left(j \left(\frac{\omega}{T} - \frac{2\pi k}{T} \right) \right)$
- Similarly, we obtain a DT filter from a CT filter by
$$h[n] = T_d h_c(nT_d)$$

Then

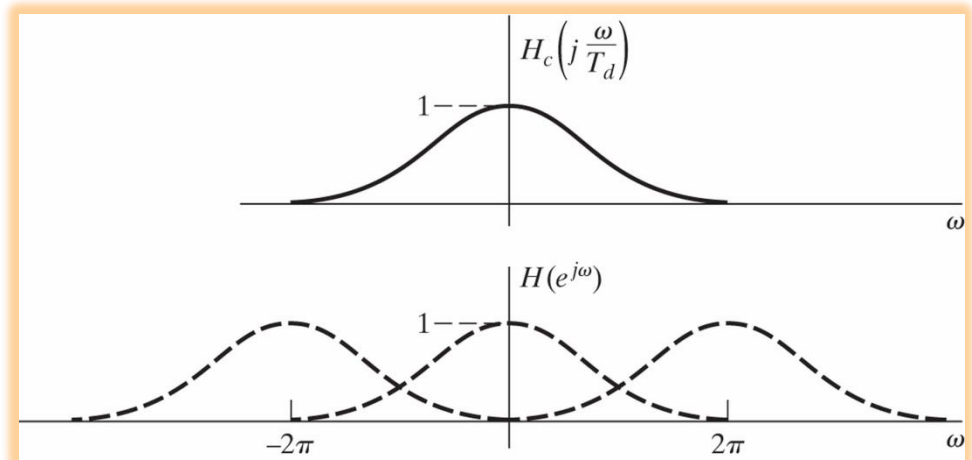
$$H(e^{j\omega}) = \sum_{k=-\infty}^{\infty} H_c \left(j \left(\frac{\omega}{T_d} - \frac{2\pi k}{T_d} \right) \right)$$

Impulse Invariance

- If the CT filter is band-limited, *i.e.* $H_c(j\Omega) = 0$ for $|\Omega| > \frac{\pi}{T_d}$,

$$H(e^{j\omega}) = H_c\left(j\frac{\omega}{T_d}\right), \quad |\omega| \leq \pi$$

- In practice, aliasing occurs and the effect should be checked after the design
- The design sampling period T_d can be set to any value
 - It does not affect the implemented filter



Impulse Invariance

- **Step 1:** Transform the DT filter specifications to CT filter specifications

$$H_c(j\Omega) = H(e^{j\Omega T_d})$$

- **Step 2:** Obtain a CT filter $H_c(s)$
- **Step 3:** $H_c(s) \Rightarrow h_c(t) \Rightarrow h[n] \Rightarrow H(z)$

- ex) $H_c(s) = \frac{A_k}{s-s_k} \Rightarrow H(z) = \frac{T_d A_k}{1-e^{s_k T_d} z^{-1}}$

- **Step 4:** Check the aliasing effect
 - If the DT specifications are not satisfied, restart with stronger constraints.

Ex) Butterworth Filter Design Using Impulse Invariance

- **Step 1:** Given DT filter specifications

$$\begin{aligned} 0.89125 \leq |H(e^{j\omega})| \leq 1, & \quad 0 \leq |\omega| \leq 0.2\pi \\ |H(e^{j\omega})| \leq 0.17783, & \quad 0.3\pi \leq |\omega| \leq \pi \end{aligned}$$

we have CT specifications with $T_d = 1$

$$\begin{aligned} 0.89125 \leq |H_c(j\Omega)| \leq 1, & \quad 0 \leq |\Omega| \leq 0.2\pi \\ |H_c(j\Omega)| \leq 0.17783, & \quad 0.3\pi \leq |\Omega| \leq \pi \end{aligned}$$

Ex) Butterworth Filter Design Using Impulse Invariance

- Step 2: Butterworth filter

$$|H_c(j\Omega)|^2 = \frac{1}{1 + \left(\frac{\Omega}{\Omega_c}\right)^{2N}}$$

$$1 + \left(\frac{0.2\pi}{\Omega_c}\right)^{2N} = \left(\frac{1}{0.89125}\right)^2 \text{ and } 1 + \left(\frac{0.3\pi}{\Omega_c}\right)^{2N} = \left(\frac{1}{0.17783}\right)^2$$

$$\Rightarrow N = 5.8858 \simeq 6 \text{ and } \Omega_c = 0.70474$$

Then, based on the CT signal processing techniques

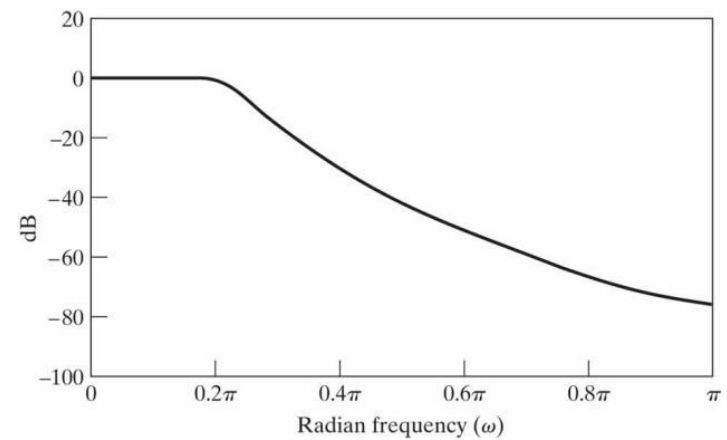
$$H_c(s) = \frac{0.12}{(s^2 + 0.36s + 0.49)(s^2 + 0.99s + 0.49)(s^2 + 1.36s + 0.49)}$$

- Step 3: Digital Butterworth filter

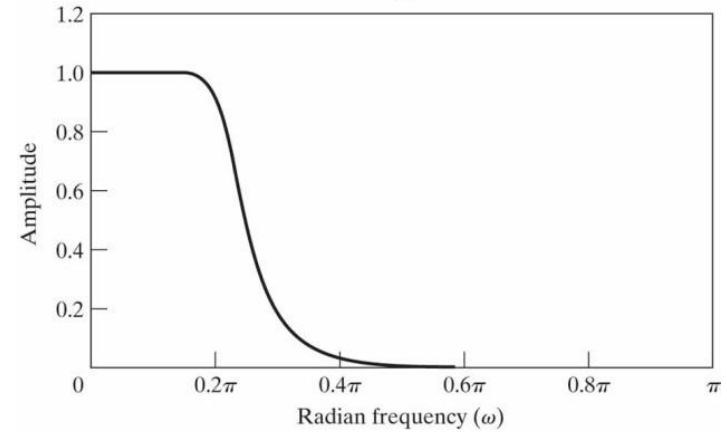
$$H(z) = \frac{0.29 - 0.45z^{-1}}{1 - 1.30z^{-1} + 0.69z^{-2}} + \frac{-2.14 + 1.15z^{-1}}{1 - 1.07z^{-1} + 0.37z^{-2}} + \frac{1.86 - 0.63z^{-1}}{1 - 1.00z^{-1} + 0.26z^{-2}}$$

Ex) Butterworth Filter Design Using Impulse Invariance

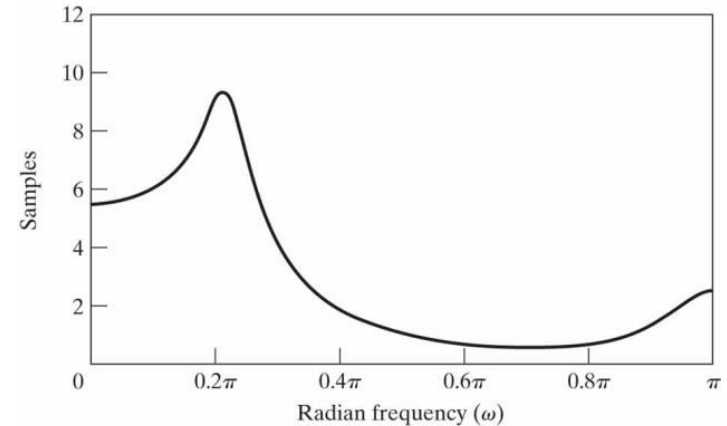
- Step 4: Check



(a)



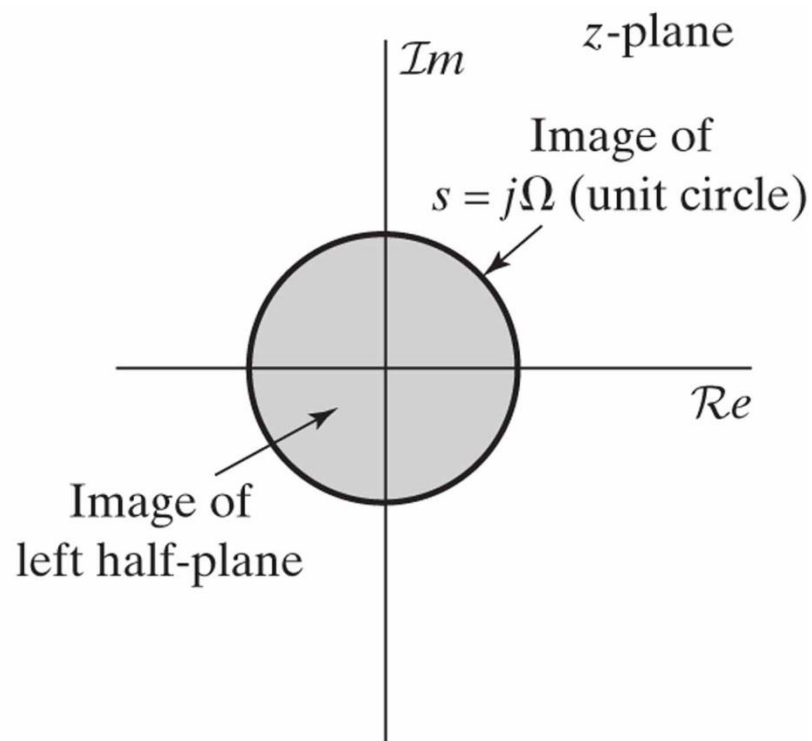
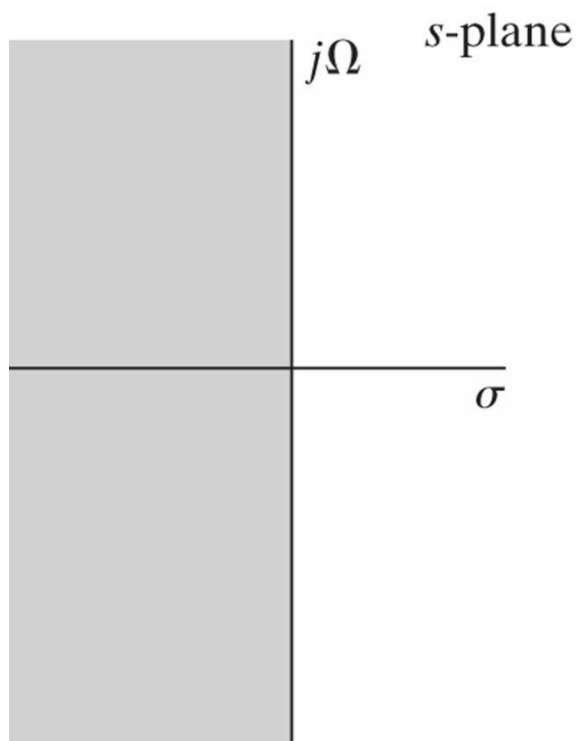
(b)



(c)

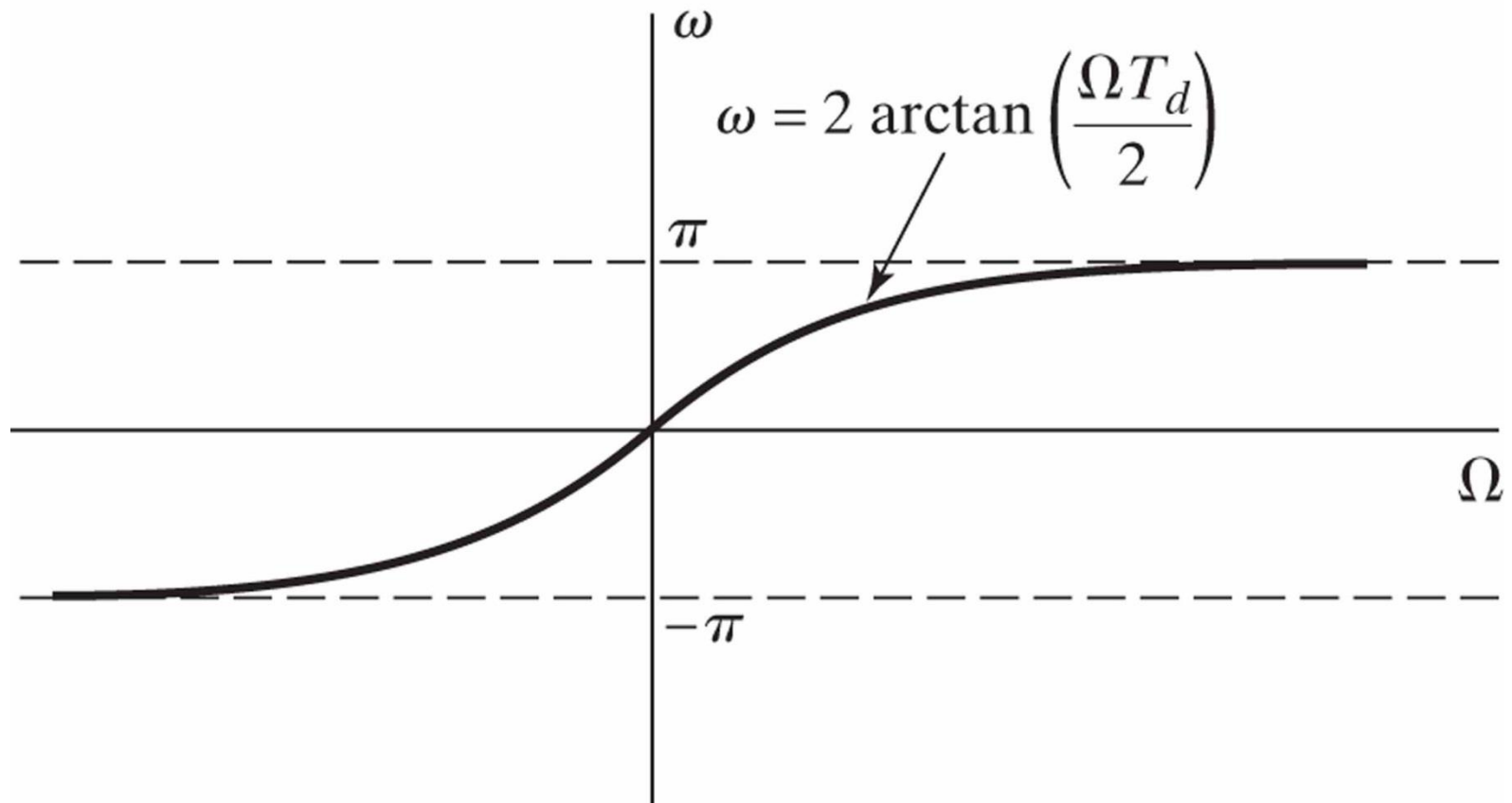
Bilinear Transformation

- $s = \frac{2}{T_d} \left(\frac{1-z^{-1}}{1+z^{-1}} \right)$ or $z = \frac{1+\frac{T_d}{2}s}{1-\frac{T_d}{2}s}$

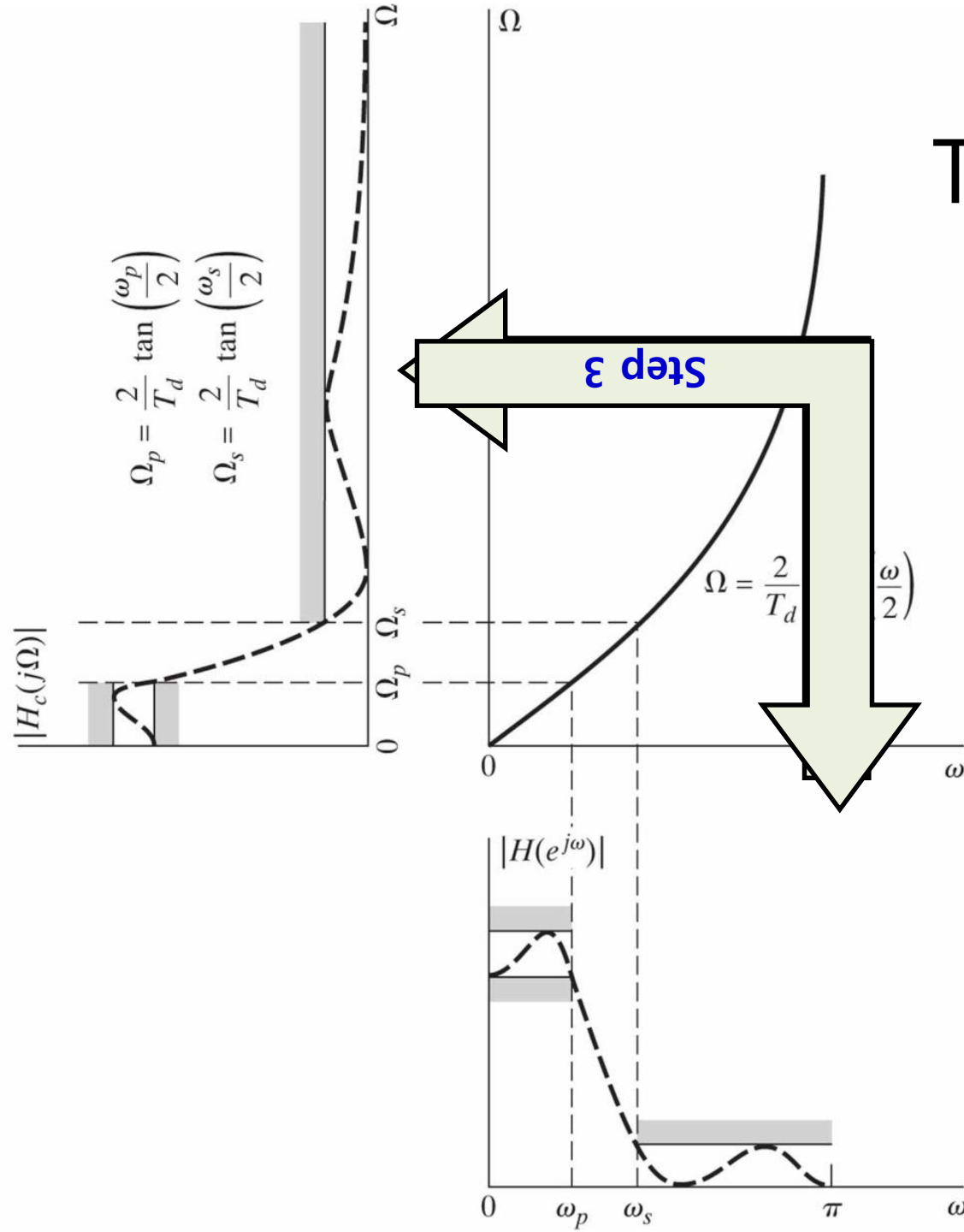


Bilinear Transformation

- $\Omega = \frac{2}{T_d} \tan\left(\frac{\omega}{2}\right)$ or $\omega = 2 \arctan\left(\frac{\Omega T_d}{2}\right)$



Bilinear Transformation



- **Step 1:** Transform the DT filter spec. to CT filter spec.

- **Step 2:** Obtain a CT filter $H_c(s)$

- **Step 3:** $H(z) = H_c\left(\frac{2}{T_d} \left(\frac{1-z^{-1}}{1+z^{-1}}\right)\right)$

Ex) Butterworth Filter Design Using Bilinear Transformation

- **Step 1:** Given DT filter specifications

$$0.89125 \leq |H(e^{j\omega})| \leq 1, \quad 0 \leq |\omega| \leq 0.2\pi$$
$$|H(e^{j\omega})| \leq 0.17783, \quad 0.3\pi \leq |\omega| \leq \pi$$

we have CT specifications with $T_d = 1$

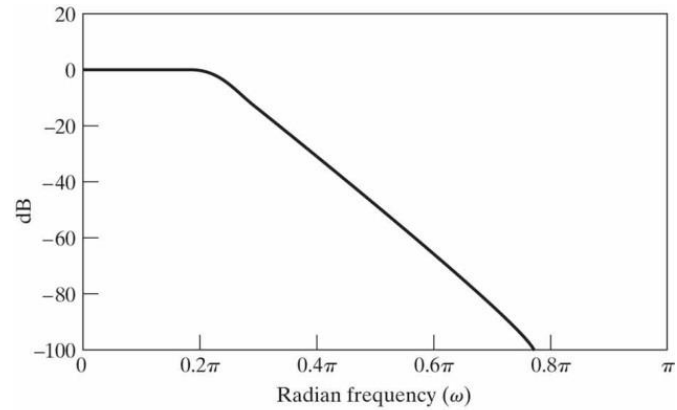
$$0.89125 \leq |H_c(j\Omega)| \leq 1, \quad 0 \leq |\Omega| \leq 2 \tan\left(\frac{0.2\pi}{2}\right)$$

$$|H_c(j\Omega)| \leq 0.17783, \quad 2 \tan\left(\frac{0.3\pi}{2}\right) \leq |\Omega| \leq \infty$$

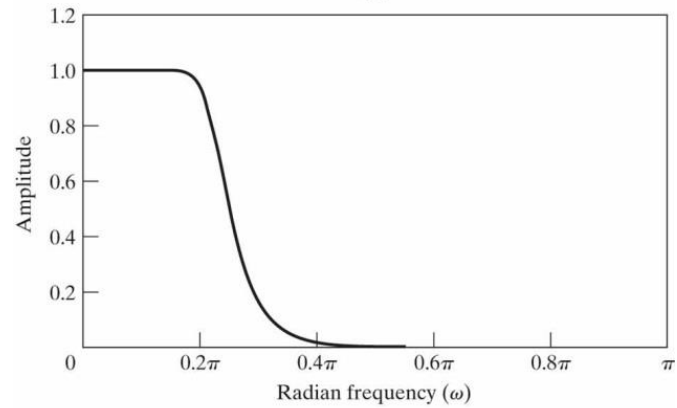
- **Step 2:** Obtain a CT Butterworth filter

- **Step 3:** $H(z) = H_c\left(2 \left(\frac{1-z^{-1}}{1+z^{-1}}\right)\right)$

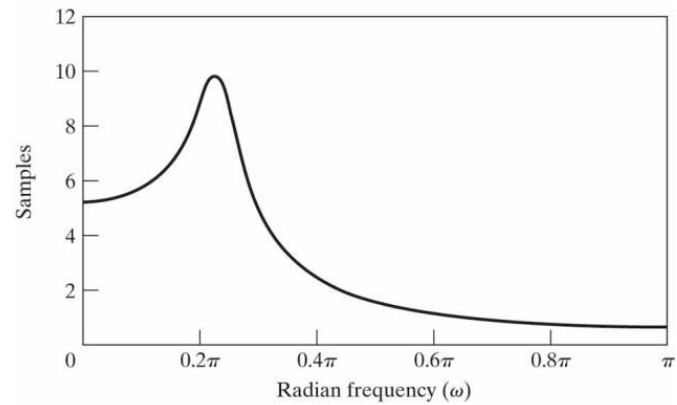
Ex) Butterworth Filter Design Using Bilinear Transformation



(a)



(b)



(c)

Comparison of Butterworth, Chebyshev, and Elliptic Filters

- Specifications
 - Passband edge frequency $\omega_p = 0.5\pi$
 - Stopband edge frequency $\omega_s = 0.6\pi$
 - Maximum passband gain = 0 dB
 - Minimum passband gain = -0.3dB
 - Maximum stopband gain = -30dB

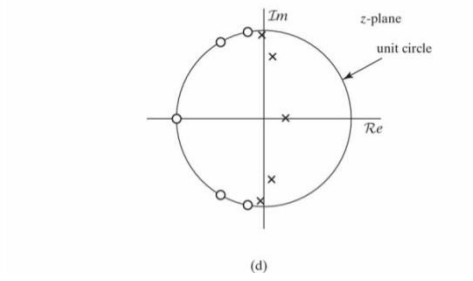
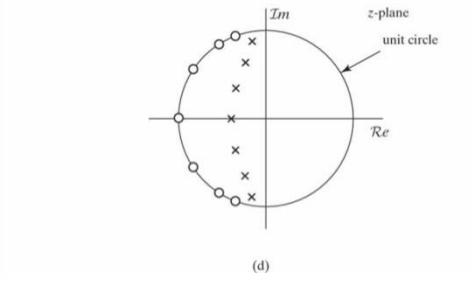
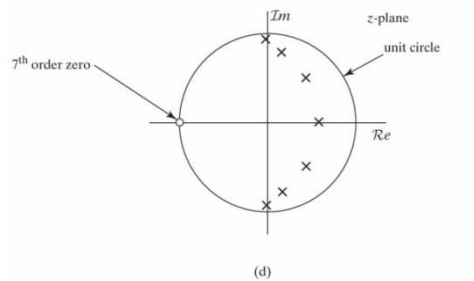
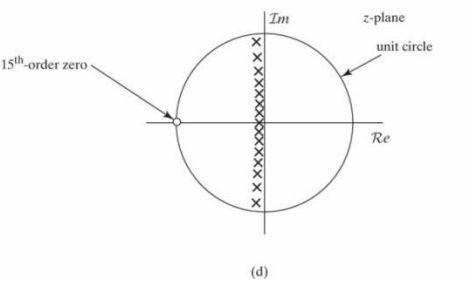
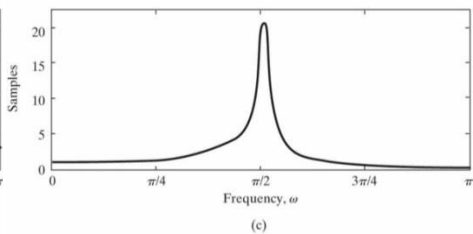
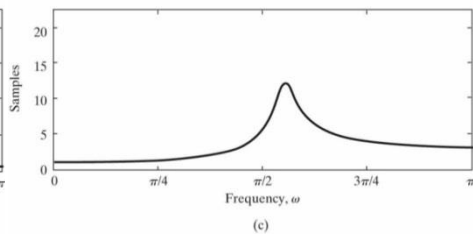
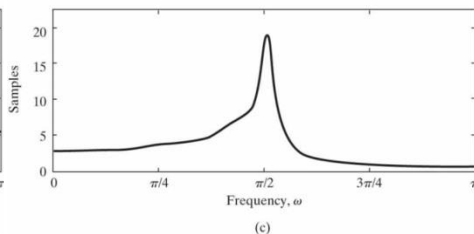
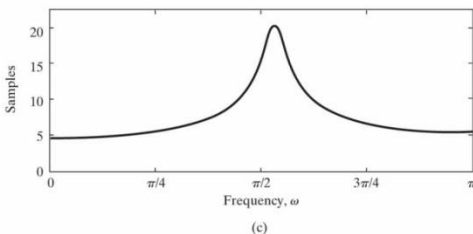
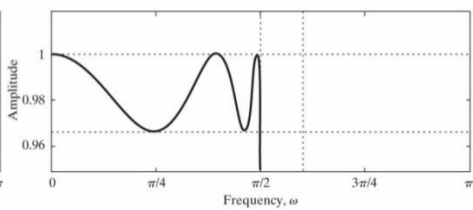
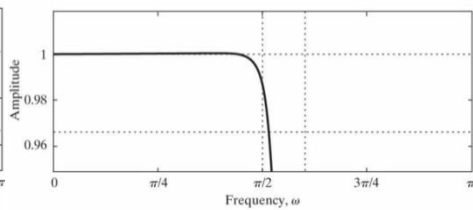
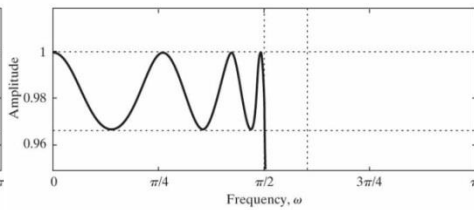
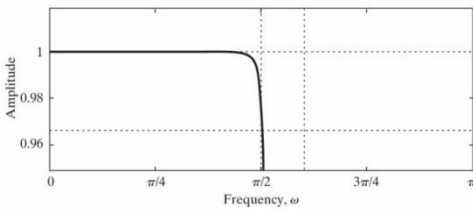
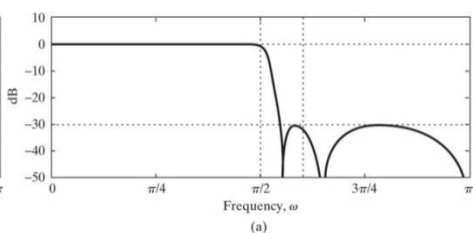
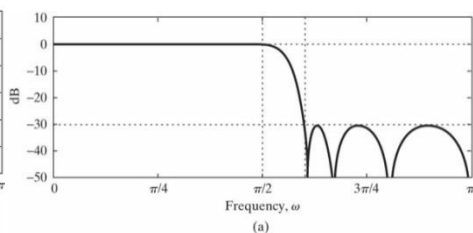
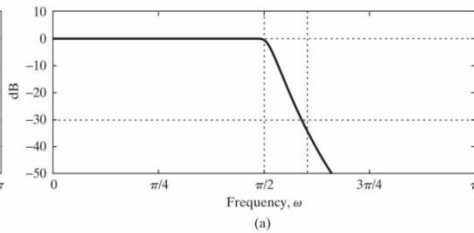
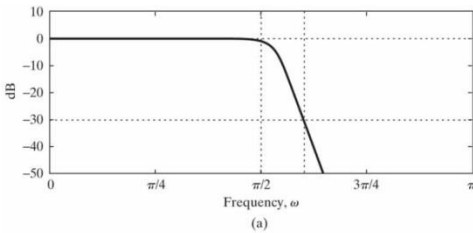
Comparison of Butterworth, Chebyshev, and Elliptic Filters

Monotone

Ripple in passband

Ripple in stopband

Ripples!



Butterworth, 15th

Chebyshev I, 7th

Chebyshev II, 7th

Elliptic, 5th